



Designation: D2171/D2171M – 18

## Standard Test Method for Viscosity of Asphalts by Vacuum Capillary Viscometer<sup>1</sup>

This standard is issued under the fixed designation D2171/D2171M; the number immediately following the designation indicates the year of original adoption or, in the case of revision, the year of last revision. A number in parentheses indicates the year of last reapproval. A superscript epsilon ( $\epsilon$ ) indicates an editorial change since the last revision or reapproval.

*This standard has been approved for use by agencies of the U.S. Department of Defense.*

*This test method has been approved by the sponsoring committees and accepted by the cooperating societies in accordance with established procedures.*

### 1. Scope

1.1 This test method covers procedures for the determination of the apparent viscosity of asphalt binder by vacuum capillary viscometers at 60 °C [140 °F]. It is applicable to materials having viscosities in the range from 0.0036 to over 20 000 Pa·s [0.036 to over 200 000 P].

NOTE 1—This test method is suitable for use at other temperatures, but the precision is based on determinations on asphalt binders at 60 °C [140 °F].

NOTE 2—Modified asphalt binders or asphalt binders that have been conditioned or recovered are typically non-Newtonian under the conditions of this test. The apparent viscosity for non-Newtonian asphalt binders varies with shear rate. When the flow is non-Newtonian in a capillary tube, the shear rate determined using this test method may be invalid. The presence of non-Newtonian behavior for the test conditions of this test can be verified by measuring the viscosity with viscometers having different-sized capillary tubes or with different pressure heads. The defined precision limits in Section 11 may not be applicable to non-Newtonian asphalt binders. Test Method D4957 may be a more applicable method for testing non-Newtonian asphalts.

1.2 The values stated in either SI units or inch-pound units are to be regarded separately as standard. The values stated in each system may not be exact equivalents; therefore, each system shall be used independently of the other. Combining values from the two systems may result in nonconformance with the standard.

1.3 **Warning**—Mercury has been designated by the United States Environmental Protection Agency (EPA) and many state agencies as a hazardous material that can cause central nervous system, kidney, and liver damage. Mercury, or its vapor, may be hazardous to health and corrosive to materials. Caution should be taken when handling mercury and mercury-containing products. See the applicable product Material Safety Data Sheet (MSDS) or Safety Data Sheet (SDS) for details and the EPA's website—<http://www.epa.gov/mercury/faq.htm>—for additional information. Users should be aware

<sup>1</sup> This test method is under the jurisdiction of ASTM Committee D04 on Road and Paving Materials and is the direct responsibility of Subcommittee D04.44 on Rheological Tests.

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that selling mercury, mercury-containing products, or both, in your state may be prohibited by state law.

1.4 The text of this standard references notes and footnotes that provide explanatory material. These notes and footnotes (excluding those in tables and figures) shall not be considered as requirements of the standard.

1.5 *This standard does not purport to address all of the safety concerns, if any, associated with its use. It is the responsibility of the user of this standard to establish appropriate safety, health, and environmental practices and determine the applicability of regulatory limitations prior to use.*

1.6 *This international standard was developed in accordance with internationally recognized principles on standardization established in the Decision on Principles for the Development of International Standards, Guides and Recommendations issued by the World Trade Organization Technical Barriers to Trade (TBT) Committee.*

### 2. Referenced Documents

2.1 *ASTM Standards*:<sup>2</sup>

D8 Terminology Relating to Materials for Roads and Pavements

D3666 Specification for Minimum Requirements for Agencies Testing and Inspecting Road and Paving Materials

D4957 Test Method for Apparent Viscosity of Asphalt Emulsion Residues and Non-Newtonian Asphalts by Vacuum Capillary Viscometer

E1 Specification for ASTM Liquid-in-Glass Thermometers

E11 Specification for Woven Wire Test Sieve Cloth and Test Sieves

E77 Test Method for Inspection and Verification of Thermometers

E879 Specification for Thermistor Sensors for General Purpose and Laboratory Temperature Measurements

E1137/E1137M Specification for Industrial Platinum Resistance Thermometers

<sup>2</sup> For referenced ASTM standards, visit the ASTM website, [www.astm.org](http://www.astm.org), or contact ASTM Customer Service at [service@astm.org](mailto:service@astm.org). For *Annual Book of ASTM Standards* volume information, refer to the standard's Document Summary page on the ASTM website.

### 3. Terminology

#### 3.1 Definitions of Terms Specific to This Standard:

3.1.1 *Newtonian viscosity,  $n$* —the viscosity of a liquid that is shear-rate independent, in which the rate of shear is linearly proportional to the shearing stress.

3.1.2 *non-Newtonian viscosity,  $n$* —the viscosity of a liquid that is shear-rate dependent, in which the rate of shear is not linearly proportional to the shearing stress.

3.1.3 *viscosity (coefficient of),  $n$* —the ratio between the applied shear stress and rate of shear is called the coefficient of viscosity.

3.1.3.1 *Discussion*—This coefficient is a measure of the resistance to flow of the liquid. It is commonly called the viscosity of the liquid. The cgs unit of viscosity is 1 g/cm·s (1 dyne·s/cm<sup>2</sup>) and is called a poise (P). The SI unit of viscosity is 1 Pa·s (1 N·s/m<sup>2</sup>) and is called a Pascal-second. One Pa·s is equivalent to 10 P.

3.2 For definitions of other terms used in this standard, refer to Terminology **D8**.

### 4. Summary of Test Method

4.1 The time is measured for a fixed volume of the liquid to be drawn up through a capillary tube by means of vacuum, under closely controlled conditions of vacuum and temperature. The viscosity in Pascal-seconds is calculated by multiplying the flow time in seconds by the viscometer calibration factor.

### 5. Significance and Use

5.1 The viscosity at 60 °C [140 °F] characterizes flow behavior and may be used for specification requirements for cutback asphalt and asphalt binders.

NOTE 3—The quality of the results produced by this standard are dependent on the competence of the personnel performing the procedure and the capability, calibration, and maintenance of the equipment used. Agencies that meet the criteria of Specification **D3666** are generally considered capable of competent and objective testing, sampling, inspection, etc. Users of this standard are cautioned that compliance with Specification **D3666** alone does not completely ensure reliable results. Reliable results depend on many factors; following the suggestions of Specification **D3666** or some similar acceptable guideline provides a means of evaluating and controlling some of those factors.

### 6. Apparatus

6.1 *Viscometers*, capillary-type, made of borosilicate glass, annealed, suitable for this test are as follows:

6.1.1 *Cannon-Manning Vacuum Viscometer (CMVV)*, as described in **Appendix X1**.

6.1.2 *Asphalt Institute Vacuum Viscometer (AIVV)*, as described in **Appendix X2**.

6.1.3 *Modified Koppers Vacuum Viscometer (MKVV)*, as described in **Appendix X3**.

6.1.4 Calibrated viscometers are available from commercial suppliers. Details regarding calibration of viscometers are given in **Appendix X4**.

NOTE 4—The viscosity measured in a CMVV may be from 1 to 5 % lower than either the AIVV or MKVV having the same viscosity range.

This difference, when encountered, may be the result of non-Newtonian flow.<sup>3</sup>

6.2 *Thermometers*—A calibrated thermometer (see **Table X5.1**) with suitable range and estimated measurement uncertainty of 0.02 °C [0.04 °F] or less at 95 % confidence interval listed on the calibration certificate and is one of the following:

6.2.1 A liquid-in-glass thermometer that is calibrated annually. The calibration shall be verified at the ice point in accordance with **Appendix X5**. ASTM Kinematic Viscosity Thermometers 47C and 47F conforming to Specification **E1** are suitable for the most commonly used temperature of 60 °C [140 °F].

NOTE 5—The specified thermometers in **6.2.1** are standardized as “total immersion” thermometers, which are designed to indicate temperatures correctly when just that portion of the thermometer containing the liquid is exposed to the temperature being measured and the remainder of the stem and expansion chamber at the top of the thermometer exposed to the room temperature. The practice of completely submerging the thermometer is not recommended. When a “total immersion” thermometer is completely submerged, corrections for each individual thermometer based on calibration under conditions of complete submergence must be determined and applied. If the thermometer is completely submerged in the bath during use, the pressure of the gas in the expansion chamber will be higher or lower than during calibration, and may cause high or low readings on the thermometer.

6.2.2 A platinum resistance thermometer (PRT) with a sensor which conforms to the requirements of Specification **E1137/E1137M**. The thermometer shall be calibrated annually as a single unit and have a three- or four-wire connection configuration. The sensing element shall be immersed to the depth specified by the manufacturer adjacent to the capillary tube.

NOTE 6—A minimum of 50 mm (2 in.) of the thermometer sheath (wire-connecting side) shall not be subjected to the bath medium unless otherwise specified by the manufacturer.

6.2.3 A thermistor thermometer with sensor, which conforms to the requirements of Specification **E879**, calibrated annually as a single unit. The sensing element of the thermistor shall be completely immersed in the bath adjacent to the capillary tube.

NOTE 7—The use of the thermometric devices specified in **6.2.2** and **6.2.3** are understood to introduce bias in the precision in this method.

6.3 *Bath*—A bath suitable for immersion of the viscometer so that the liquid reservoir or the top of the capillary, whichever is uppermost, is at least 20 mm below the upper surface of the bath liquid and with provisions for visibility of the viscometer and the thermometer. Firm supports for the viscometer shall be provided. The efficiency of the stirring and the balance between heat losses and heat input must be such that the temperature of the bath medium does not vary by more than  $\pm 0.03$  °C [ $\pm 0.05$  °F] over the length of the viscometer, or from viscometer to viscometer in the various bath positions.

6.4 *Vacuum System*—A vacuum system capable of maintaining a vacuum to within  $\pm 0.5$  mm Hg of the desired level up to and including 40.0 kPa [300 mm Hg]. The essential system is

<sup>3</sup> Supporting data have been filed at ASTM International Headquarters and may be obtained by requesting Research Report RR:D04-1003. Contact ASTM Customer Service at service@astm.org.

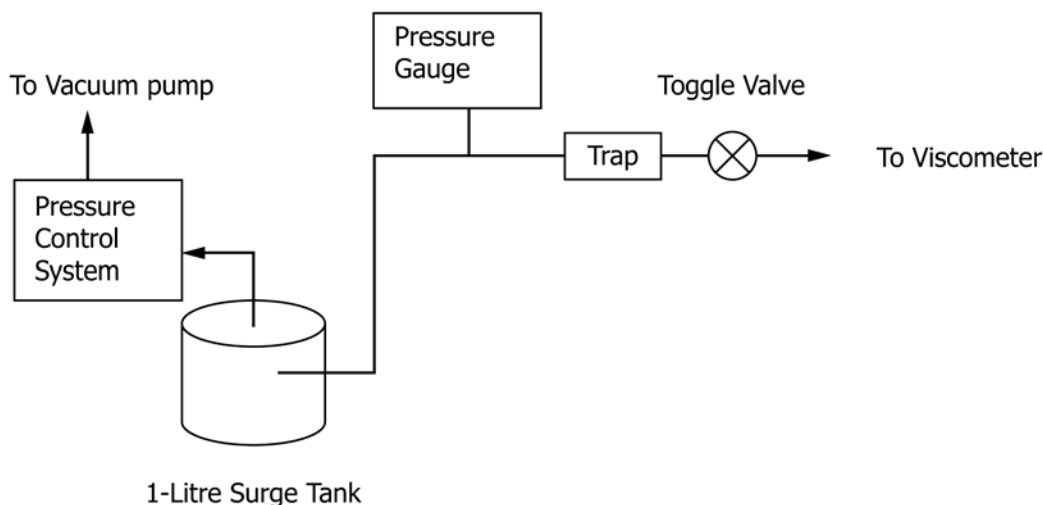


FIG. 1 Suggested Vacuum System for Vacuum Capillary Viscometers

shown schematically in Fig. 1. Tubing of 6.35-mm [ $\frac{1}{4}$ -in.] inside diameter should be used, and all joints should be airtight so that when the system is closed, no loss of vacuum is indicated by the pressure gauge. A vacuum or aspirator pump is suitable for the vacuum source. The vacuum measuring system for this test method must be standardized at least once a year.

6.5 *Timer*—A stopwatch or other timing device graduated in divisions of 0.1 s or less and accurate to within 0.05 % when tested over intervals of not less than 15 min. Timing devices for this test method must be standardized at least every twelve months.

6.5.1 *Electrical Timing Devices* may be used only on electrical circuits, the frequencies of which are controlled to an accuracy of 0.05 % or better.

6.5.1.1 Alternating currents, the frequencies of which are intermittently and not continuously controlled, as provided by some public power systems, can cause large errors, particularly over short timing intervals, when used to actuate electrical timing devices.

## 7. Sample Preparations

7.1 Heat the sample with care to prevent local overheating until it has become sufficiently fluid to pour, occasionally stirring the sample to aid heat transfer and to ensure uniformity.

7.2 Transfer a minimum of 20 mL into a suitable container and heat to  $135 \pm 5.5$  °C [ $275 \pm 10$  °F], stirring occasionally to prevent local overheating and taking care to avoid the entrapment of air.

NOTE 8—If it is suspected that the sample may contain solid material, strain the melted sample into the container through a 300- $\mu$ m [No. 50] sieve conforming to Specification E11.

NOTE 9—In the case of very viscous or modified asphalts, it may be necessary to heat in an oven at  $163 \pm 5$  °C [ $325 \pm 10$  °F] in order for the material to become sufficiently fluid to stir and pour.

## 8. Procedure

8.1 The specific details of operation vary somewhat for the various types of viscometers. See the detailed descriptions of

viscometers in Appendix X1 – Appendix X3 for instructions for using the type of viscometer selected. In all cases, however, follow the general procedure described in 8.1.1 – 8.1.9.

8.1.1 Maintain the bath at the test temperature within  $\pm 0.03$  °C [ $0.05$  °F]. Apply the necessary corrections, if any, to all thermometer readings.

8.1.2 Select a clean, dry viscometer that will give a flow time greater than 60 s, and preheat to  $135 \pm 5.5$  °C [ $275 \pm 10$  °F].

8.1.3 Charge the viscometer by pouring the prepared sample to within  $\pm 2$  mm of fill line E (Figs. 2-4).

8.1.4 Place the charged viscometer in an oven or bath maintained at  $135 \pm 5.5$  °C [ $275 \pm 10$  °F] for a period of  $10 \pm 2$  min, to allow large air bubbles to escape.

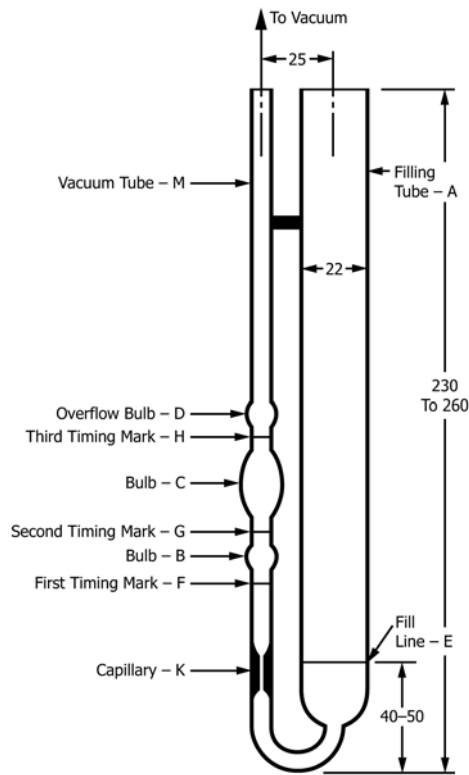
8.1.5 Remove the viscometer from the oven or bath and, within 5 min, insert the viscometer in a holder, and position the viscometer vertically in the bath so that the uppermost timing mark is at least 20 mm below the surface of the bath liquid.

8.1.6 Establish a  $40.0 \pm 0.07$  kPa [ $300 \pm 0.5$  mm Hg] vacuum below atmospheric pressure in the vacuum system and connect the vacuum system to the viscometer with the toggle valve or stopcock closed in the line leading to the viscometer.

8.1.7 After the viscometer has been in the bath for  $30 \pm 5$  min, start the flow of asphalt in the viscometer by opening the toggle valve or stopcock in the line leading to the vacuum system.

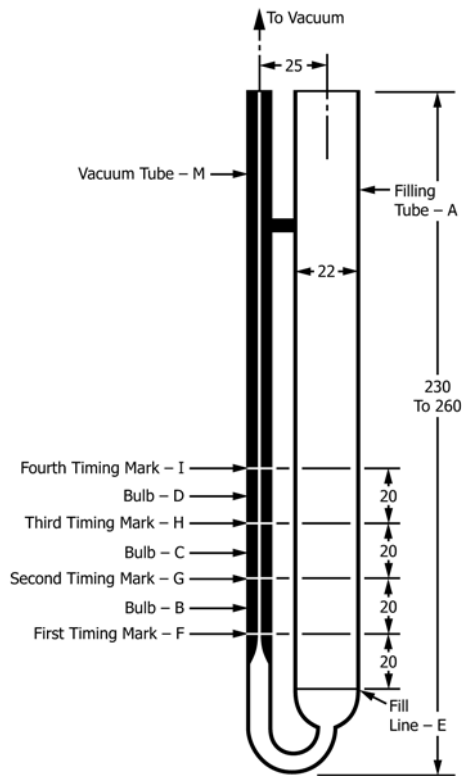
8.1.8 Measure to within 0.1 s the time required for the leading edge of the meniscus to pass between successive pairs of timing marks. Report the first flow time which exceeds 60 s between a pair of timing marks, noting the identification of the pair of timing marks.

8.1.9 Upon completion of the test, clean the viscometer thoroughly by several rinsings with an appropriate solvent completely miscible with the sample, followed by a completely volatile solvent. Dry the tube by passing a slow stream of filtered dry air through the capillary for 2 min, or until the last trace of solvent is removed. Alternatively, the viscometer may be cleaned in a glass-cleaning oven, at a temperature not to exceed 500 °C [ $932$  °F], followed by rinses with distilled or



All dimensions are in millimetres.

FIG. 2 Cannon-Manning Vacuum Capillary Viscometer



All dimensions are in millimetres.

FIG. 3 Asphalt Institute Vacuum Capillary Viscometer

deionized water, residue-free acetone, and filtered dry air. Periodically, if deposits are observed, clean the instrument with a strong acid cleaning solution to remove organic deposits, rinse thoroughly with distilled or deionized water and residue-free acetone, and dry with filtered dry air.

8.1.9.1 Chromic acid cleaning solution may be prepared by adding, with the usual precautions, 800 mL of concentrated sulphuric acid to a solution of 92 g of sodium dichromate in 458 mL of water. The use of similar commercially available sulphuric acid cleaning solutions is acceptable. Nonchromium-containing, strongly oxidizing acid cleaning solutions may be substituted so as to avoid the disposal problems of chromium-containing solutions.

8.1.9.2 Use of alkaline glass-cleaning solutions may result in a change of viscometer calibration, and is not recommended.

### 9. Calculation

9.1 Select the calibration factor that corresponds to the pair of timing marks used for the determination, as prescribed in 8.1.8. Calculate and report the viscosity to three significant figures using the following equation:

$$\text{Viscosity, Pa}\cdot\text{s} = (Kt) \tag{1}$$

where:

$K$  = selected calibration factor, Pa·s/s, and  
 $t$  = flow time, s.

NOTE 10—If the viscometer constant or calibration factor ( $K_{cgs}$ ) is known in cgs units (Poise/s) calculate the calibration factor ( $K_{si}$ ) in SI units (pascal-seconds/second) as follows:

$$K_{si} = (\text{Pa}\cdot\text{s}/\text{s}) = K_{cgs}/10 \text{ or } (P/\text{s})/10 \tag{2}$$

### 10. Report

10.1 Always report the test temperature and vacuum with the viscosity test result.

NOTE 11—For example, viscosity at 60 °C [140 °F] and 40.0 kPa [300 mm Hg] vacuum, in Pa·s.

### 11. Precision and Bias

11.1 The following criteria (see Note 1) should be used for judging the acceptability of results (95 % probability):

11.1.1 *Repeatability*—Duplicate results by the same operator using the same viscometer should not be considered suspect unless they differ by more than 7 % of their mean.

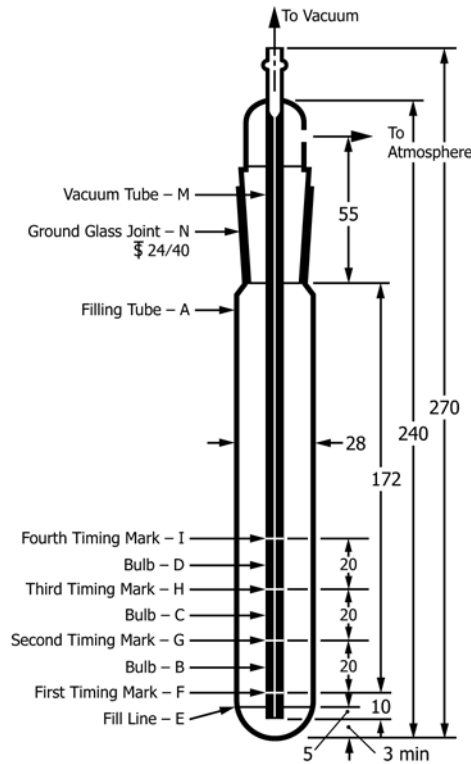
11.1.2 *Reproducibility*—The results submitted by each of two laboratories should not be considered suspect unless the two results differ by more than 10 % of their mean.

NOTE 12—Supporting data and information for determining these estimates can be found in Manning, R. E., “Comments on Vacuum Viscometers for Measuring the Viscosity of Asphalt Cements,” *Symposium on Fundamental Viscosity of Bituminous Materials*, ASTM STP 328, ASTM International, 1963, pp. 44–47.

11.2 *Bias*—The bias for this test method cannot be determined because no material with an accepted reference value is available.

### 12. Keywords

12.1 asphalt; capillary; vacuum; viscometer; viscosity



All dimensions are in millimetres.

FIG. 4 Modified Koppers Vacuum Capillary Viscometer

APPENDIXES

(Nonmandatory Information)

X1. CANNON-MANNING VACUUM CAPILLARY VISCOMETER (CMVV)

X1.1 Scope

X1.1.1 The Cannon-Manning vacuum capillary viscometer (CMVV)<sup>4,5</sup> is available in eleven sizes (Table X1.1) covering a range from 0.0036 to 8 000 Pa·s [0.036 to 80 000 P]. Sizes 10 through 14 are best suited to viscosity measurements of asphalt cements at 60 °C [140 °F].

X1.2 Apparatus

X1.2.1 Details of the design and construction of Cannon-Manning vacuum capillary viscometers are shown in Fig. 2. The size numbers, approximate bulb factors, *K*, and viscosity ranges for the series of Cannon-Manning vacuum capillary viscometers are given in Table X1.1.

X1.2.2 For all viscometer sizes, the volume of measuring bulb *C* is approximately three times that of bulb *B*.

TABLE X1.1 Standard Viscometer Sizes, Approximate Calibration Factors, *K* and Viscosity Ranges for Cannon-Manning Vacuum Capillary Viscometers

Viscometer Size Number	Approximate Calibration Factor, <i>K</i> <sup>A</sup> 40 kPa [300 mm Hg] Vacuum, Pa·s/s (P/s/10)		Viscosity Range, Pa·s <sup>B</sup>	Viscosity Range, P <sup>B</sup>
	Bulb B	Bulb C		
4	0.0002	0.0006	0.0036 to 0.08	0.036 to 0.8
5	0.0006	0.002	0.012 to 0.24	0.12 to 2.4
6	0.002	0.006	0.036 to 0.8	0.36 to 8
7	0.006	0.02	0.12 to 2.4	1.2 to 24
8	0.02	0.06	0.36 to 8	3.6 to 80
9	0.06	0.2	1.2 to 24	12 to 240
10	0.2	0.6	3.6 to 80	36 to 800
11	0.6	2.0	12 to 240	120 to 2 400
12	2.0	6.0	36 to 800	360 to 8 000
13	6.0	20.0	120 to 2 400	1 200 to 24 000
14	20.0	60.0	360 to 8 000	3 600 to 80 000

<sup>A</sup> Exact calibration factors must be determined with viscosity standards.

<sup>B</sup> The viscosity ranges shown in this table correspond to a filling time of 60 to 400 s. Longer flow times (up to 1000 s) may be used.

<sup>4</sup> Griffith, J. M. and Puzinauskas, V. P., "Relation of Empirical Tests to Fundamental Viscosity of Asphalt Cement and the Relative Precision of Data Obtained by Various Tests Methods," *Symposium on Fundamental Viscosity of Bituminous Materials*, ASTM STP 328, ASTM International, 1963, pp. 20–44.

<sup>5</sup> Manning, R. E., "Comments on Vacuum Viscometers for Measuring the Viscosity of Asphalt Cements," *Symposium on Fundamental Viscosity of Bituminous Materials*, ASTM STP 328, ASTM International, 1963, pp. 44–47.

X1.2.3 A convenient holder can be made by drilling two holes, 22 and 8 mm in diameter, respectively, through a No. 11

rubber stopper. The center-to-center distance between holes should be 25 mm. Slit through the rubber stopper between holes and also between the 8-mm hole and edge of the stopper.

When placed in a 50-mm [2-in.] diameter hole in the bath cover, the stopper holds the viscometer in place. Such holders are commercially available.

## X2. ASPHALT INSTITUTE VACUUM CAPILLARY VISCOMETER (AIVV)

### X2.1 Scope

X2.1.1 The Asphalt Institute vacuum capillary viscometer (AIVV)<sup>4,5</sup> is available in seven sizes (Table X2.1) from a range from 4.2 to 580 000 Pa·s [42 to 5 800 000 P]. Sizes 50 through 200 are best suited to viscosity measurements of asphalt cements at 60 °C [140 °F].

### X2.2 Apparatus

X2.2.1 Details of design and construction of the Asphalt Institute vacuum capillary viscometer are shown in Fig. 3. The size numbers, approximate radii, approximate bulb factors, *K*, and viscosity range for the series of Asphalt Institute vacuum capillary viscometers are given in Table X2.1.

X2.2.2 This viscometer has measuring bulbs, *B*, *C*, and *D*, located on the viscometer arm, *M*, which is a precision-bore glass capillary. The measuring bulbs are 20-mm-long capillary segments, separated by timing marks, *F*, *G*, *H*, and *I*.

X2.2.3 A convenient holder can be made by drilling two holes, 22 and 8 mm in diameter, respectively, through a No. 11 rubber stopper. The center-to-center distance between holes should be 25 mm. Slit through the rubber stopper between the holes and also between the 8-mm hole and edge of the stopper. When placed in a 50-mm [2-in.] diameter hole in the bath cover, the stopper holds the viscometer in place. Such holders are commercially available.

**TABLE X2.1 Standard Viscometer Sizes, Capillary Radii, Approximate Calibration Factors, *K*, and Viscosity Ranges for Modified Koppers Vacuum Capillary Viscometers**

Viscometer Size Number	Approximate Capillary Radius, mm	Approximate Calibration Factor, <i>K</i> , <sup>A</sup> 40 kPa [300 mm] Hg Vacuum, Pa·s/s (P/s)/10			Viscosity Range, Pa·s <sup>B</sup>	Viscosity Range, P <sup>B</sup>
		Bulb B	Bulb C	Bulb D		
25	0.125	0.2	.1	0.07	4.2 to 80	42 to 800
50	0.25	0.8	.4	.3	18 to 320	180 to 3 200
100	0.50	3.2	1.6	1.0	60 to 1 280	600 to 12 800
200	1.0	12.8	6.4	4.0	240 to 5 200	2 400 to 52 000
400	2.0	50.0	25.0	16.0	960 to 20 000	9 600 to 200 000
400R <sup>C</sup>	2.0	50.0	25.0	16.0	960 to 140 000	9 600 to 1 400 000
800R <sup>C</sup>	4.0	200.0	100.0	64.0	3 800 to 580 000	38 000 to 5 800 000

<sup>A</sup> Exact calibration factors must be determined with viscosity standards.

<sup>B</sup> The viscosity ranges shown in this table correspond to a filling time of 60 to 400 s. Longer flow times (up to 1000 s) may be used.

<sup>C</sup> Special design for roofing asphalts having additional marks at 5 and 10 mm above timing mark, *F* (see Fig. 3). Thus, using these marks, the maximum viscosity range is increased from that using the bulb *B* calibration factor.

### X3. MODIFIED KOPPERS VACUUM CAPILLARY VISCOMETER (MKVV)

#### X3.1 Scope

X3.1.1 The Modified Koppers vacuum capillary viscometer (MKVV)<sup>6,7,8</sup> is available in five sizes (Table X3.1) covering a range from 4.2 to 20 000 Pa·s [42 to 200 000]. Sizes 50 through 200 are best suited to viscosity measurements of asphalt cements at 60 °C [140 °F].

#### X3.2 Apparatus

X3.2.1 Details of design and construction of the Modified Koppers vacuum capillary viscometer are shown in Fig. 4. The

<sup>6</sup> Rhodes, E. O., Volkmann, E. W., and Barker, C. T., “New Viscometer for Bitumens Has Extended Range,” *Engineering News-Record*, Vol 115, No. 21, 1935, p. 714.

<sup>7</sup> Lewis, R. H. and Halstead, W. J., “Determination of the Kinematic Viscosity of Petroleum Asphalts with a Capillary Tube Viscometer,” *Public Roads*, Vol 21, No. 7, September 1940, p. 127.

<sup>8</sup> Heithaus, J. J., “Measurement of Asphalt Viscosity with a Vacuum Capillary Viscometer,” *Papers on Road and Paving Materials and Symposium on Microviscometry*, ASTM STP 309, ASTM International, 1961, p. 63.

size numbers, approximate radii, approximate bulb factors,  $K$ , and viscosity ranges for the series of Modified Koppers vacuum capillary viscometers are given in Table X3.1.

X3.2.2 This viscometer consists of a separate filling tube,  $A$ , and precision-bore glass capillary vacuum tube,  $M$ . These two parts are joined by a borosilicate ground glass joint,  $N$ , having a 24/40 standard taper. The measuring bulbs  $B$ ,  $C$ , and  $D$ , on the glass capillary are 20-mm-long capillary segments, separated by timing marks  $F$ ,  $G$ ,  $H$ , and  $I$ .

X3.2.3 A viscometer holder can be made by drilling a 28-mm hole through the center of a No. 11 rubber stopper and slitting the stopper between the hole and the edge. When placed in a 50-mm [2-in.] diameter hole in the bath cover, it holds the viscometer in place.

**TABLE X3.1 Standard Viscometer Sizes, Capillary Radii, Approximate Calibration Factors,  $K$ , and Viscosity Ranges for Modified Koppers Vacuum Capillary Viscometers**

Viscometer Size Number	Approximate Capillary Radius, mm	Approximate Calibration Factor, $K$ , <sup>A</sup> 40 kPa [300 mm] Hg Vacuum, Pa·s/s (P/s)/10			Viscosity Range, Pa·s <sup>B</sup>	Viscosity Range, Pa·s <sup>B</sup>
		Bulb B	Bulb C	Bulb D		
25	0.125	0.2	0.1	0.07	4.2 to 80	42 to 800
50	0.25	0.8	0.4	0.3	18 to 320	180 to 3 200
100	0.50	3.2	1.6	1.0	60 to 1 280	600 to 12 800
200	1.0	12.8	6.4	4.0	240 to 5 200	2 400 to 52 000
400	2.0	50.0	25.0	16.0	960 to 20 000	9 600 to 200 000

<sup>A</sup> Exact calibration factors must be determined with viscosity standards.

<sup>B</sup> The viscosity ranges shown in this table correspond to a filling time of 60 to 400 s. Longer flow times (up to 100 s) may be used.

## X4. CALIBRATION OF VISCOMETERS

**TABLE X4.1 Viscosity Standards**

Viscosity Standard	Approximate Viscosity, Pa·s			Approximate Viscosity, P		
	At 25 °C	At 40 °C	At 60 °C	At 25 °C	At 40 °C	At 60 °C
	[77 °F]	[104 °F]	[140 °F]	[68 °F]	[104 °F]	[140 °F]
N30000 <sup>A</sup>	80	...	4.7	800	...	47
N190000 <sup>A</sup>	520	140	33	5200	1400	330
N2700000 <sup>A</sup>	5300	...	340	53000	...	3400
S30000 <sup>A</sup>	71	20	...	710	200	...

<sup>A</sup> Available in 1-pt containers.

### X4.1 Scope

X4.1.1 This appendix describes the materials and procedures used for calibrating or checking the calibration of viscometers used in this method.

### X4.2 Reference Materials

X4.2.1 *Viscosity Standards* having approximate viscosities are given in [Table X4.1](#).

### X4.3 Calibration

X4.3.1 *Calibration of Vacuum Viscometer by Means of Viscosity Standards*—Calibrate the vacuum viscometer as follows:

X4.3.1.1 Select from [Table X4.1](#) a viscosity standard having a minimum flow time of 60 s at the calibration temperature.

X4.3.1.2 Charge a clean, dry viscometer by pouring the sample to within  $\pm 2$  mm of fill line *E* (see [Figs. 2-4](#)).

X4.3.1.3 Place the charged viscometer in the viscometer bath, maintained at the calibration temperature  $\pm 0.01$  °C [ $\pm 0.02$  °F].

X4.3.1.4 Establish a  $40.0 \pm 0.07$  kPa [ $300 \pm 0.5$  mm] Hg vacuum in the vacuum system and connect the vacuum system to the viscometer with the toggle valve or stopcock closed in the line leading to the viscometer.

X4.3.1.5 After the viscometer has been in the bath for 30  $\pm$  5 min, start the flow of standard in the viscometer by opening the stopcock or toggle valve in the line leading to the vacuum system.

X4.3.1.6 Measure to within 0.1 s the time required for the leading edge of the meniscus to pass between timing marks *F* and *G*. Using a second timer, also measure to within 0.1 s the

time required for the leading edge of the meniscus to pass between timing marks *G* and *H*. If the instrument contains additional timing marks, similarly determine the flow time for each successive bulb.

X4.3.1.7 Calculate the calibration factor, *K*, for each bulb as follows:

$$K = \eta/t \quad (\text{X4.1})$$

where:

*K* = viscometer bulb calibration factor, at 40.0 kPa [300 mm] (Pa·s/s),

$\eta$  = viscosity of viscosity standard at calibration temperature, Pa·s, and

*t* = flow time, s.

X4.3.1.8 Repeat the calibration procedure using the same viscosity standard or another viscosity standard. Record the average calibration constant, *K*, for each bulb.

NOTE X4.1—The duplicate determinations of calibration constant, *K*, for each bulb **must** agree with 2 % of their mean ([Note X4.2](#)).

NOTE X4.2—The bulb constants are independent of temperature.

X4.3.2 *Calibration of Vacuum Viscometer by Means of Standard Vacuum Viscometer*—Calibrate the vacuum viscometer as follows:

X4.3.2.1 Select any petroleum asphalt having a flow time of at least 60 s. Select also a standard viscometer of known bulb constants.

X4.3.2.2 Mount the standard viscometer together with the viscometer to be calibrated in the same bath at 60 °C [140 °F] and determine the flow times of the asphalt by the procedure described in [8.1](#).

X4.3.2.3 Calculate the constant, *K*, for each bulb as follows:

$$K_1 = (t_2 \times K_2)/t_1 \quad (\text{X4.2})$$

where:

*K*<sub>1</sub> = constant of viscometer bulb being calibrated,

*t*<sub>1</sub> = flow time of viscometer bulb being calibrated,

*K*<sub>2</sub> = bulb constant of standard viscometer, and

*t*<sub>2</sub> = flow time of corresponding bulb in standard viscometer.



## X5. ICE POINT DETERMINATION AND RECALIBRATION OF LIQUID-IN-GLASS KINEMATIC VISCOSITY THERMOMETERS

**TABLE X5.1 Kinematic Viscosity Test Thermometers<sup>A</sup>**

Test Temperature Scale Error <sup>B</sup>		Thermometer Number	
°C	°F	ASTM <sup>C</sup>	IP <sup>D</sup>
20 and 21.1	68 and 70	44C, F	29C, F
25	77	45C, F	30C, F
30	86	118C, F	...
37.8	100	28F	31C, F
40		120C	...
50	122	46C, F	66C, F
54.4	130	29F	34C, F
60	140	47C, F	35C, F
82.2	180	48F	90C, F
93.3	200	...	36C, F
98.9 and 100	210 and 212	30F	32C, F
100		121C	
135	275	110C, F	

<sup>A</sup> The smallest graduation of the Celsius thermometers is 0.05 °C and for the Fahrenheit thermometers is 0.1 °F.

<sup>B</sup> Scale error for the Celsius thermometers is not to exceed ±0.1 °C for the Fahrenheit thermometers it is ±0.2 °F (except for ASTM 110F which is ±0.3°F). These scale errors are required to apply only at the given test temperature.

<sup>C</sup> Complete construction detail is given in Specification E1.

<sup>D</sup> Complete construction detail is given in Part I of IP Standards for Petroleum and its Products.

X5.1 To achieve an accuracy of ±0.02 °C [±0.04 °F] for calibrated liquid-in-glass kinematic viscosity thermometers, it is required that a check at the ice point be made and the corrections altered for the change seen in the ice point. It is recommended that the interval of checking be every six months; for a new thermometer, check monthly for the first six months.

X5.2 A detailed procedure for the measurement of the ice point and recalibration of thermometers is described in 6.5 of Test Method E77. The suggestions in the following sections of this appendix are given specifically for the mercury-in-glass kinematic viscosity thermometers described in Table X5.1, and may not apply to other thermometers.

X5.2.1 The ice point reading of liquid-in-glass kinematic viscosity thermometers shall be taken within 60 min after being at the test temperature for not less than 3 min. The ice point reading shall be expressed to the nearest 0.01 °C or 0.02 °F.

X5.2.2 Select clear pieces of ice, preferably made from distilled or pure water. Discard any cloudy or unsound portions. Rinse the ice with distilled water and shave or crush into

small pieces, avoiding direct contact with the hands or any chemically unclean objects. Fill the Dewar vessel with the crushed ice and add sufficient distilled and preferably pre-cooled water to form a slush, but not enough to float the ice. As the ice melts, drain off some of the water and add more crushed ice. Insert the thermometer, packing the ice gently about the stem, to a depth approximately one scale division below the 0 °C [32 °F] graduation. It may be necessary to repack the ice around the thermometer because of melting.

X5.2.3 After at least 3 min have elapsed, tap the stem gently and observe the reading. Successive readings taken at least 1 min apart should agree within one tenth of a division.

X5.2.4 Record the ice point reading and compare it with the previous reading. If the reading is found to be higher or lower than the reading corresponding to a previous calibration, readings at all other temperatures will be correspondingly increased or decreased.

X5.2.5 The ice point procedure given in X5.1 – X5.2.4 is used for the recalibration of liquid-in-glass kinematic viscosity thermometers, and a complete new calibration of the thermometer is not necessary in order to meet the accuracy ascribed to this design thermometer.

X5.3 It is recommended that these kinematic viscosity thermometers be stored vertically when not in use so as to avoid the separation of the liquid column.

X5.4 It is recommended that these kinematic viscosity thermometers be read to the nearest one fifth of a division using appropriate magnification. Since these thermometers are typically in a kinematic viscosity bath (which has vision through the front), the thermometer is read by lowering the thermometer such that the top of the liquid column is 5 to 15 mm below the surface of the bath liquid. Be careful to ensure that the expansion chamber at the top of the thermometer is above the lid of the constant temperature bath. If the expansion chamber is at elevated or lowered temperatures from ambient temperatures, a significant error can occur. This error can be as much as one or two thermometer divisions. A reading glass such as used for reading books may be useful to ensure reading the scale to one fifth of a division.



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